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## Method for revamping a combined blast furnace and air gas separation unit system

The present invention relates to a method for revamping a combined system consisting of a blast furnace supplied with oxidizing fluid issuing at least partially from an air gas separation unit (ASU).

enrich an air stream with oxygen, the production of high purity oxygen is not required, the use of a distillation apparatus comprising a mixing column as described in document US-A-4 022 (Brugerolle) is suitable. Combined systems consisting of a blast furnace and an air distillation apparatus comprising such a mixing column are described, example, in documents US-A-5 244 489 (Grenier) EP-A-0 531 182 in the name of the applicant. the approaches followed in these two documents are opposed: in document US-A-5 244 489, the distillation apparatus is fully supplied with air by a branch of the stream from a blast furnace blower, and the portion of air stream supplied by the mixing column slightly pressurized by a booster driven by a coldmaintaining turbine that expands the portion of the air stream sent to the medium pressure column, which, to effect said pressurizing, arrangement requires a large part of the air feed for the medium pressure column to pass through the turbine, causing extraction yield and energy losses, and also oversizing of the cooling and cleaning stations for the air feed to the distillation apparatus. Conversely, document EP-A-0 531 182 provides for a complete separation of the air feeds a) to the blast furnace b) to the medium pressure column and c) to the mixing column, compression means for, in separate particular, producing impure oxygen at high or low pressures in the mixing column, in an arrangement that is costly in terms of investment and operation of rotating machines,

and does not provide for any synergy between these units.

EP-A-0 932 006 proposes a combined system and a method for using such an intensively integrated combined system and obtaining substantially lower operating costs, while offering flexibility in selecting the operating ranges.

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For this purpose, the proposed method is of the type comprising at least one furnace supplied with air by at least one blower supplying air at a first pressure P<sub>1</sub>, and with oxygen supplied by at least one air distillation apparatus comprising at least one medium pressure column at least partially supplied with air by the furnace blower, and a mixing column supplying the oxygen to the furnace, and in which the mixing column is supplied with air by a compressor compressing the air to a pressure P<sub>2</sub> higher than P<sub>1</sub>.

According to a particular feature, the medium pressure column is supplied exclusively with compressed air supplied by the furnace blower.

Within the framework of environmental conservation programs, use is often made of oxycombustion in the boilers because of the higher efficiency of this type of process (the nitrogen present in the air is not heated needlessly and a gas very rich in  $CO_2$  and containing very little  $N_2$  can be recovered directly) and because of the limitation of  $NO_x$  emissions, particularly by the combustion of industrially pure oxygen (above 90% oxygen).

For the blast furnace, this is hence reflected by the injection of pure oxygen (or oxygen diluted with air) in order to obtain over 50% by volume of oxygen in the stream sent to the blast furnace, preferably over 80% oxygen and more preferably over 90 vol% oxygen.

However, a conventional air blast furnace features an air blower with a potentially extremely high flow rate at a pressure equal to or greater than  $2.5 \times 10^5$  pascals, which is little needed, if at all, in a "highly oxygenated oxygen stream" process as described above.

In fact, either no air at all is injected into the blast furnace, or a very small quantity (less than 25% of the capacity of the blower or blowers) is injected to dilute the oxygen, leaving a blower which operates below its minimum capacity, requiring it to produce more and to recycle the surplus production, or to discharge the surplus to the atmosphere, which is a poor and extremely costly solution in terms of energy in both cases.

The technical problem to be solved hence consists in efficiently and economically reusing an air blower available on the blast furnace site.

The proposed solution consists in controlling this blower flow rate and/or pressure by a controller of which the measurement and setpoint derive from the ASU (typically from the cleaning unit (inlet or outlet air flow rate), or from the precooling (air flow rate between blower outlet and cleaning inlet), or from the suction of a second machine (suction pressure of an additional compressor)).

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The method of the invention is characterized in that more than 50% of the flow from the blower feeding the blast furnace before revamping is injected into a cryogenic air gas separation unit in order to produce oxygen with a purity above 90% by volume of  $O_2$  fed to the blast furnace, the blower air flow rate and/or pressure of the air issuing from the blower being controlled by a controller which measures this flow rate and/or pressure at the inlet and/or outlet of the

air cleaning stage, placed upstream of the separation unit, in order to control the flow rate or pressure of the air issuing from the blower, the blast furnace feed fluid consisting of pure oxygen or oxygen diluted with air produced by the cryogenic separation unit.

According to the invention, the air is supplied in part or in full by at least one blast furnace blower, the air flow thus supplied accounting for over 50% of the compressed air flow delivered by said at least one blower.

At least one blower flow rate and/or pressure is preferably controlled by a controller of which the measurement and setpoint derive from the ASU (typically from the cleaning unit (inlet or outlet air flow rate), or from the precooling (air flow rate between blower outlet and cleaning inlet)).

According to a first variant of the invention, the air is supplied in part or in full by at least one blast furnace blower, the air flow thus supplied accounting for over 50% of the air flow compressed by the blower(s), while at least one blower flow rate is controlled by a controller of which the setpoint is calculated from the flow rate of one of the products issuing from the ASU (oxygen, nitrogen and/or argon in liquid or gaseous form).

Preferably, the compressed air issuing from the blower is cooled to a temperature of 50°C or lower, and then, optionally, recompressed in a second compressor or blower, before being sent to a cleaning unit upstream of the ASU.

According to another variant of the invention, the blower flow rate is controlled by a FIC controller of which the measurement and setpoint derive from the ASU

(typically from the cleaning unit (inlet or outlet air

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flow rate), or from the precooling (air flow rate between blower outlet and cleaning inlet)), while the additional compressor does not comprise any specific flow control.

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According to another variant of the invention, the blower is controlled by a PIC controller of which the measurement and setpoint are applied to the fluid (air) at the recompressor suction, while the additional compressor is controlled by a FIC controller of which the measurement and setpoint derive from the ASU (typically from the cleaning unit (inlet or outlet air flow rate) or from the precooling (air flow rate between blower outlet and cleaning inlet)).

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Finally, the ASU can also produce (in gaseous or liquid form) oxygen and/or nitrogen and/or argon and/or "instrument" air for a use other than the blast furnace.

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According to one variant, the method of invention is characterized in that the blower controlled by a PIC controller of which the rate or measurement and the setpoint value determined from the fluid entering the second compressor.

The invention will be better understood from the following embodiments provided as nonlimiting examples, jointly with the figures which show:

- Figure 1, an illustration of the invention;
- Figure 2, a variant of Figure 1; and
- Figure 3, a variant of the invention with a second compressor or blower.

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In Figure 1, the compressed air from the blower 1 is sent via the line 2 into cooling means 3 and then via the line 5 to the "top" cleaning unit connected by the line 6 to the ASU 9 which delivers oxygen via the

line 10 to the blast furnace 11, at point 12. A FIC controller 7 controls the blower 1 via the electrical connections 8 and 13, by the method described above.

5 In Figure 2, which is a variant of Figure 1, the same elements have the same numerals. The control parameters are measured here in the oxygen stream entering the blast furnace, via the oxygen flow controller 14, connected to an instrument 15 which 10 calculates the setpoint FYof the FIC controls, via 18 and 13, the flow rate and/or pressure of the air delivered by the blower 1 to the cleaning unit 5.

Figure 3 shows a variant of the preceding figures with the injection of cooled air at 3 into the recompressor 19 which supplies the cleaning unit 5. The FIC controller 21 on line 6, measures the flow rate and/or pressure of the air at this particular point (as in Figure 1) and transmits the data via 23 and 24 to the recompressor 19. Another PIC controller 25 measures the flow rate and/or pressure of the air leaving the cooling means 3 and controls the blower 1 via 26 and 13 as described above.